

### Snowflake divertor configuration studies for NSTX-Upgrade

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November 15, 2011

53rd Annual Meeting of the APS Division of Plasma Physics Salt Lake City, UT, United States November 14, 2011 through November 18, 2011

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### Snowflake divertor configuration studies for **NSTX-Upgrade**

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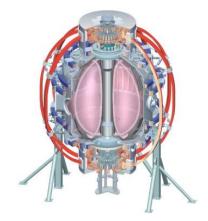
S. P. Gerhardt, R. Kaita, E. Kolemen, H. W. Kugel,

J. E. Menard (PPPL),

R. Maingi, A. G. McLean (ORNL),

and NSTX Research Team

53rd Annual Meeting of the APS Division of Plasma Physics November 14–18, 2011, Salt Lake City, Utah





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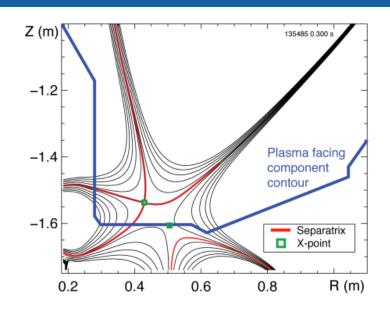
# Snowflake divertor experiments in NSTX provide basis for PMI development toward NSTX-Upgrade

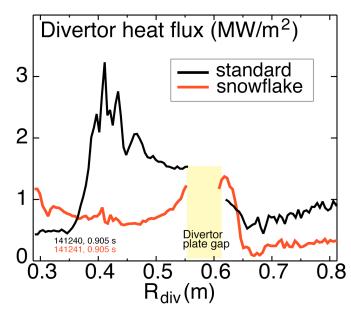
#### Snowflake divertor configuration in NSTX

- Three divertor coils, steady-state up to 600 ms
- Core H-mode confinement unchanged
- Core impurities reduced
- Steady-state divertor peak heat flux significantly reduced
  - Due to geometry effects and radiative detachment

### Development of snowflake divertor configuration for NSTX-U

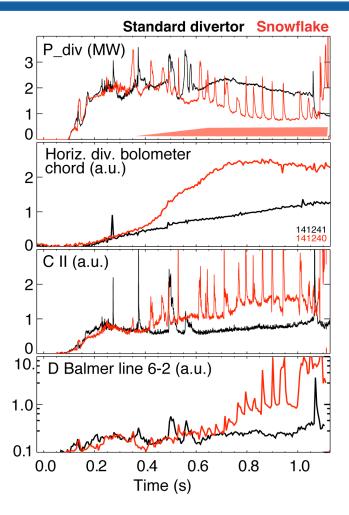
- Steady-state and transient heat flux mitigation and detachment
- Magnetic control and configuration development

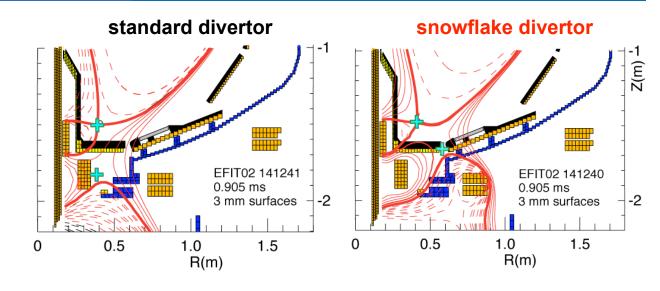






## Snowflake configuration formation was followed by radiative detachment

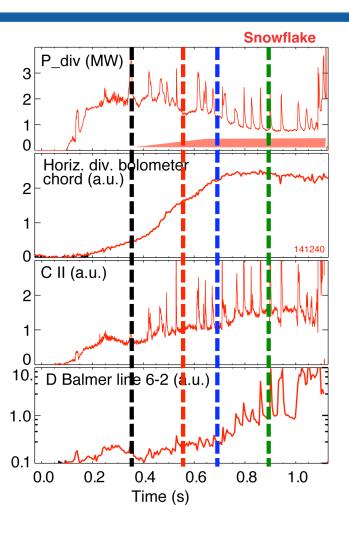


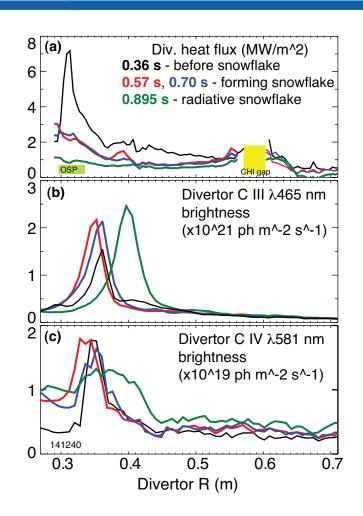


- $P_{SOL} \sim 3 \text{ MW } (P_{NBI} = 4 \text{ MW})$
- Attached divertor -> snowflake transition (still attached) -> snowflake + detachment
- $Q_{div} \sim 2 \text{ MW}$  ->  $Q_{div} \sim 1-1.2 \text{ MW}$  ->  $Q_{div} \sim 0.5-0.7 \text{ MW}$



### Significant reduction of steady-state divertor heat flux observed in snowflake divertor



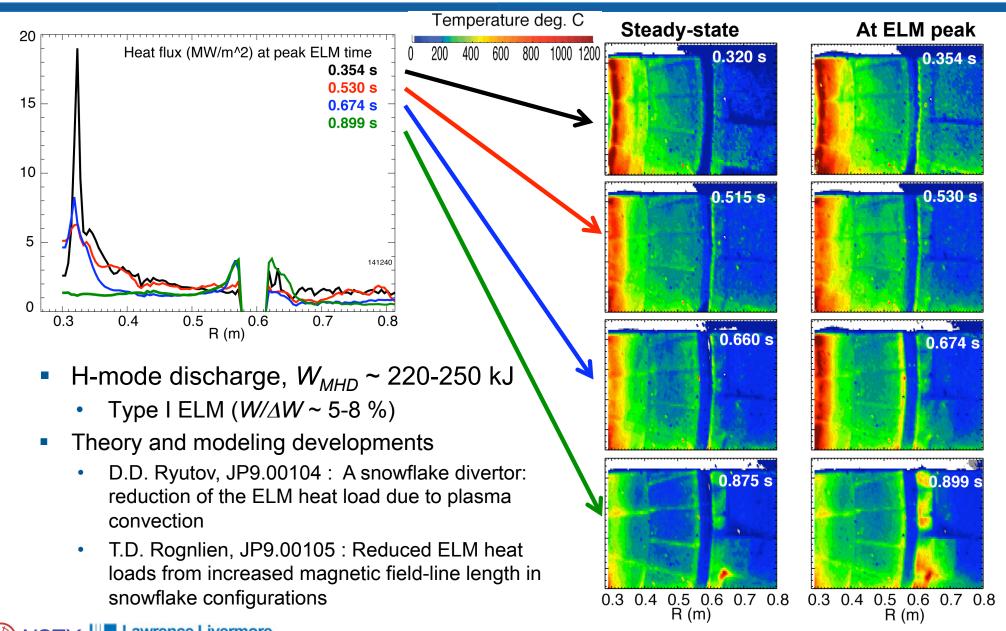


C III, CIV profiles courtesy of F. Scotti

- Attached standard divertor -> snowflake transition -> snowflake + detachment
- More experiments and modeling needed to understand geometry vs radiative effects

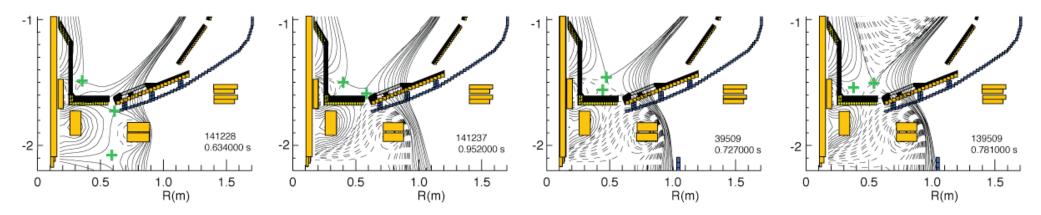


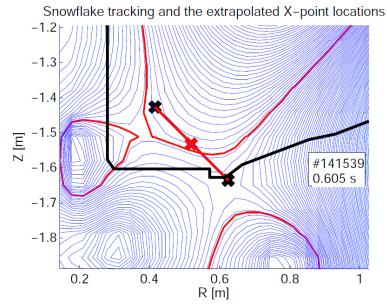
# Impulsive heat loads due to Type I ELMs are partially mitigated in snowflake divertor





# Magnetic control of snowflake divertor configuration is being developed





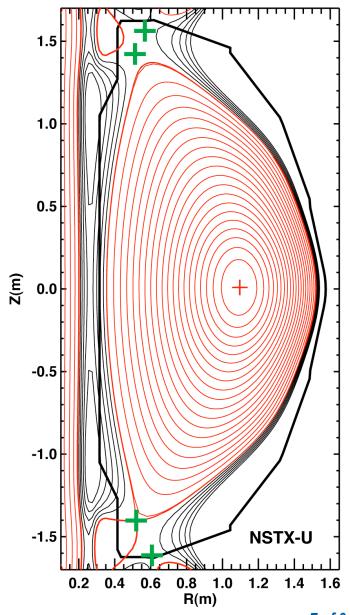
M.A. Makowski and D. Ryutov, "X-Point Tracking Algorithm for the Snowflake Divertor"

- Many ways for the open-loop snowflake configuration to fail - need close-loop feedback control of coil currents
- Testing X-point tracking algorithm
  - Locate X-points and snowflake centroid
  - E. Kolemen, PP9.00022 : Control
     Development for NSTX and the Effects of Strong Shaping
- Implementation of 2<sup>nd</sup> X-point position control in Plasma Control System being considered
  - Collaboration between PPPL, LLNL and GA



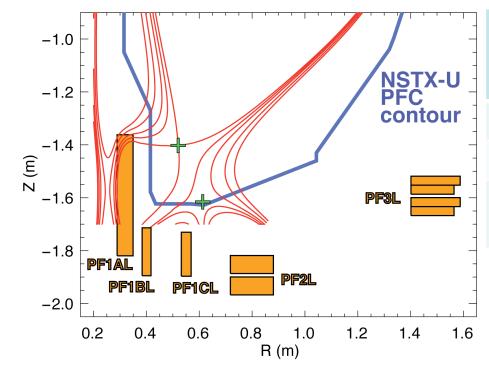
### Plasma material interface development is critical for NSTX-U success

- NSTX-U mission elements:
  - Advance ST as candidate for Fusion Nuclear Science Facility
  - Develop solutions for PMI
  - Advance toroidal confinement physics for ITER and beyond
  - Develop ST as fusion energy system
- Challenge for NSTX-U divertor
  - 2-3 X higher input power
    - $-P_{NBI}$  < 12 MW,  $I_p$  < 2 MA
  - 30-50 % reduction in n/n<sub>G</sub>
  - 3-5 X longer pulse duration
- Projected NSTX-U peak divertor heat fluxes up to 25-40 MW/m<sup>2</sup>
  - Radiative divertor with impurity seeding, double null, high flux expansion (snowflake)



# Four divertor coils should enable flexibility in boundary shaping and control in NSTX-U

- A variety of lower and both lower and upper divertor snowflake configurations are possible in NSTX-U with four coils per divertor
  - ISOLVER free-boundary Grad-Shafranov solver used
  - Four coils can be used to control up to four parameters (X-pts, OSP, etc)



Midplane flux surface	0.0	1.5 mm	3.0 mm	6.0 mm	9.0 mm
$L_{tot}(m)$	38.3	20.4	13.9	9.9	8.3
$L_X$ (m)	16.5	4.0	2.2	1.6	1.5
Angle (deg.)	1.6	8.0	0.99	3.0	3.9

 X 2 in plasma wetted surface area and connection length vs standard divertor



## Snowflake divertor experiments in NSTX provide good basis for PMI development in NSTX-Upgrade

#### FY 2009-2010 snowflake divertor experiments in NSTX

- Helped understand control of magnetic properties
- Core H-mode confinement unchanged
- Core and edge carbon concentration reduced
- Divertor heat flux significantly reduced
  - Steady-state reduction due to geometry and radiative detachment
  - Encouraging results for transient heat flux handling
  - Combined with impurity-seeded radiative divertor

#### Outlook for snowflake divertor in NSTX-Upgrade

- 2D fluid modeling of snowflake divertor properties scaling
  - Edge and divertor transport, radiation, detachment threshold
  - Compatibility with cryo-pump and lithium conditioning
- Magnetic control development
- PFC development PFC alignment and PFC material choice



### **Backup slides**



#### **Acknowledgements**

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D. D. Ryutov, T. D. Rognlien, M. V. Umansky (LLNL),
M. G. Bell, R. E. Bell, D. A. Gates, A. Diallo, S. P. Gerhardt,
R. Kaita, S. M. Kaye, E. Kolemen, B. P. LeBlanc, J. E. Menard,
D. Mueller, S. F. Paul, M. Podesta, A. L. Roquemore,
F. Scotti (PPPL),
J.-W. Ahn, R. Maingi, A. McLean (ORNL),
D. Battaglia, T. K. Gray (ORISE),
R. Raman (U Washington),
S. A. Sabbagh (Columbia U)
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Supported by the U.S. DOE under Contracts DE-AC52-07NA27344, DE AC02-09CH11466, DE-AC05-00OR22725, DE-FG02-08ER54989.

### Radiative and geometric mitigation of divertor heat flux will be needed for high-power density NSTX-Upgrade discharges

$$q_{pk} \simeq \frac{P_{heat} (1 - f_{rad}) f_{out/tot} f_{down/tot} (1 - f_{pfr}) \sin \alpha}{2\pi R_{SP} f_{exp} \lambda_{q_{||}}}$$

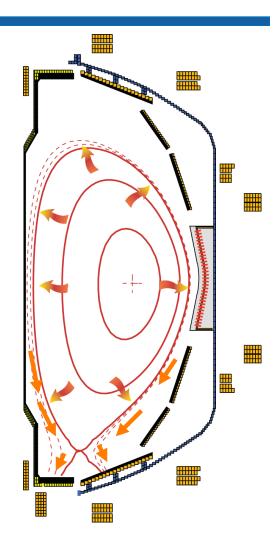
$$A_{wet} = 2\pi R f_{exp} \lambda_{q_{\parallel}} \qquad f_{exp}$$

$$f_{exp} = \frac{(B_p/B_{tot})_{MP}}{(B_p/B_{tot})_{OSP}}$$

- Radiative divertor with impurity seeding
- Double null configurations
- Snowflake configuration as laboratory of divertor physics

# Poloidal divertor concept enabled progress in tokamak physics studies in the last 30 years

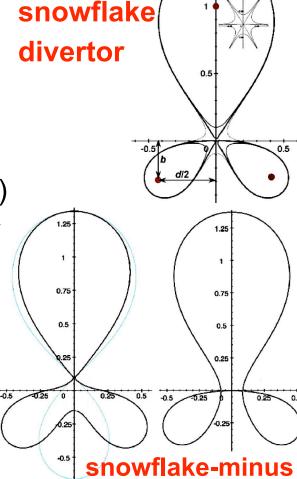
- Divertor challenge
  - Steady-state heat flux
    - present limit  $q_{peak}$  ≤ 10 MW/m<sup>2</sup>
    - projected to  $q_{peak}$  ≤ 80 MW/m<sup>2</sup> for future devices
  - Density and impurity control
  - Impulsive heat and particle loads
  - Compatibility with good core plasma performance
- Spherical tokamak: additional challenge compact divertor
- NSTX (Aspect ratio A=1.4-1.5)
  - $I_p \le 1.4 \text{ MA}, P_{in} \le 7.4 \text{ MW (NBI)}, P / R \sim 10$
  - $q_{peak} \le 15 \text{ MW/m}^2$ ,  $q_{||} \le 200 \text{ MW/m}^2$
  - Graphite PFCs with lithium coatings



**National Spherical Torus Experiment** 

# Snowflake divertor geometry attractive for heat flux mitigation

- Snowflake divertor
  - Second-order null
    - $B_p \sim 0$  and grad  $B_p \sim 0$  (Cf. first-order null:  $B_p \sim 0$ )
  - Obtained with existing divertor coils (min. 2)
  - Exact snowflake topologically unstable
- Predicted geometry properties (cf. standard divertor)
  - Larger region with low  $B_p$  around X-point: ped. stability
  - Larger plasma wetted-area  $A_{wet}$ : reduce  $q_{div}$
  - Larger X-point connection length  $L_x$ : reduce  $q_{II}$
  - Larger effective divertor volume  $V_{div}$ : incr.  $P_{rad}$ ,  $P_{CX}$
- Experiments
  - TCV (F. Piras et. al, PRL 105, 155003 (2010))
  - NSTX



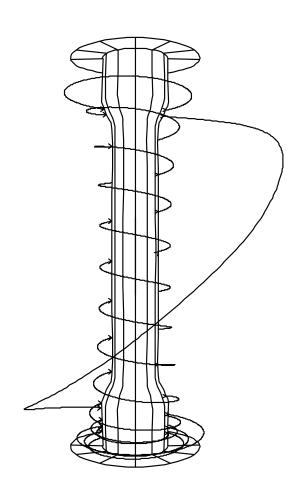
snowflake-plus

**Exact** 

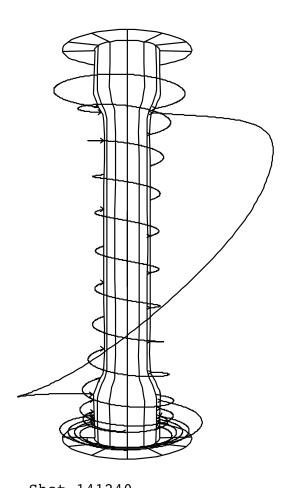
D. D. Ryutov, PoP 14, 064502 2007



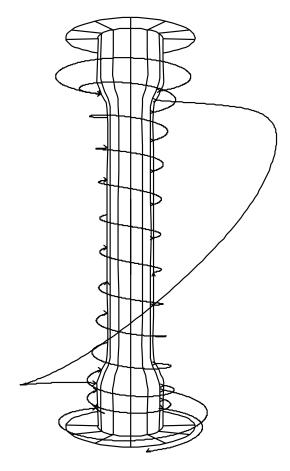
## Connection length is increased x 2-3 in snowflake divertor w.r.t. standard divertor



Shot 141241, EFIT02, time: 0.905s, normalized flux: 1.005

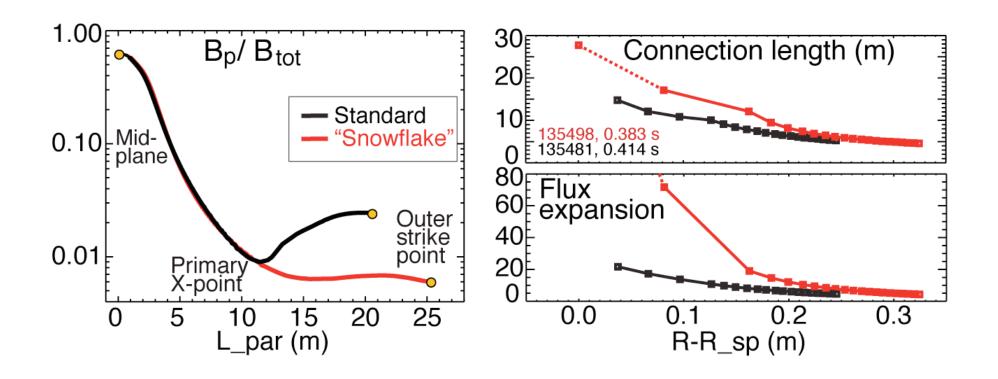


Shot 141240, EFIT02, time: 0.905s, normalized flux: 1.005



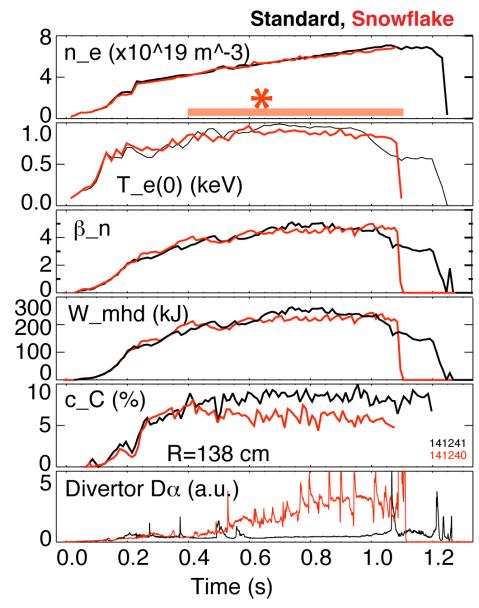
Shot 141240, EFIT02, time: 0.905s, normalized flux: 1.015

# Plasma-wetted area and connection length are increased by 50-90 % in NSTX snowflake divertor



- These properties observed in first 30-50 % of SOL width
- $B_{tot}$  angles in the strike point region: 1-2°, sometimes < 1°
  - Concern for hot-spot formation and sputtering from divertor tile edges

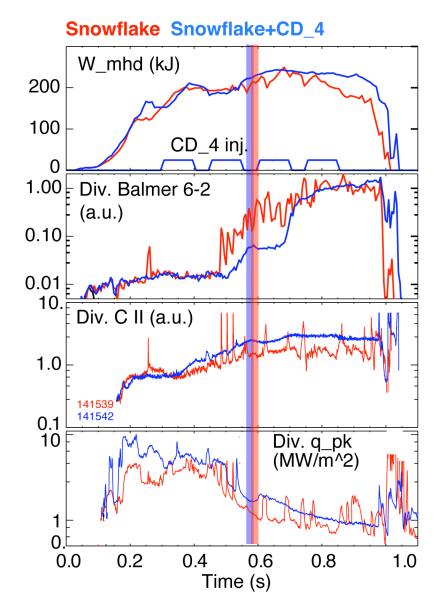
## Good H-mode confinement properties and core impurity reduction obtained with snowflake divertor



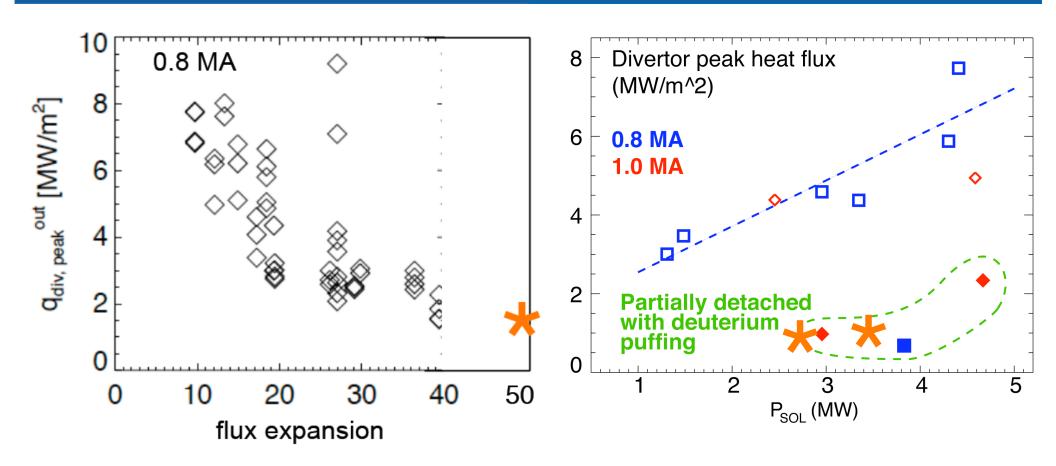
- 0.8 MA, 4 MW H-mode
- $\kappa$ =2.1,  $\delta$ =0.8
- Core  $T_e \sim 0.8$ -1 keV,  $T_i \sim 1$  keV
- $\beta_N \sim 4-5$
- Plasma stored energy ~ 250 kJ
- H98(y,2) ~ 1 (from TRANSP)
- Core carbon reduction due to
  - Type I ELMs
  - Edge source reduction
    - Divertor sputtering rates reduced due to partial detachment

## Snowflake divertor with CD<sub>4</sub> seeding leads to increased divertor carbon radiation

- $I_p$ =0.9 MA,  $P_{NBI}$ =4 MW,  $P_{SOL}$ =3 MW
- Snowflake divertor (from 0.6 ms)
  - Peak divertor heat flux reduced from 4-6 MW/m² to 1 MW/m²
- Snowflake divertor (from 0.6 ms)
   + CD<sub>4</sub>
  - Peak divertor heat flux reduced from 4-6 MW/m<sup>2</sup> to 1-2 MW/m<sup>2</sup>
  - Divertor radiation increased further



# Snowflake divertor heat flux consistent with NSTX divertor heat flux scalings

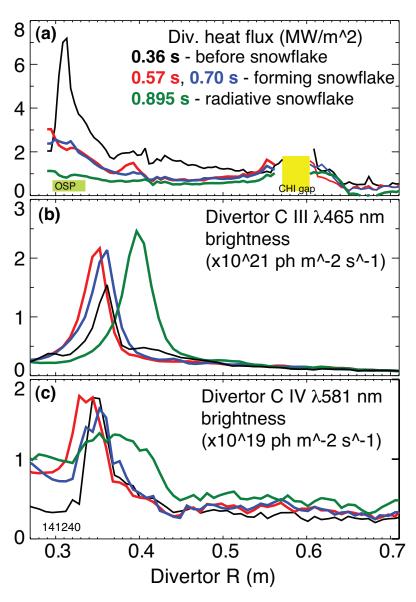


- Snowflake divertor (\*):  $P_{SOL}$ ~3-4 MW,  $f_{exp}$ ~40-60,  $q_{peak}$ ~0.5-1.5 MW/m<sup>2</sup>
  - Low detachment threshold

T. K. Gray et. al, EX/D P3-13, IAEA FEC 2010 V. A. Soukhanovskii et. al, PoP 16, 022501 (2009)



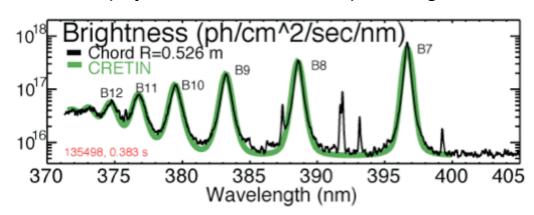
## Divertor profiles show low heat flux, broadened C III and C IV radiation zones in the snowflake divertor phase



- Heat flux profiles reduced to nearly flat low levels, characteristic of radiative heating
- Divertor C III and C IV brightness profiles broaden
- High-n Balmer line spectroscopy and CRETIN code modeling confirm outer SP detachment with T<sub>e</sub> ≤ 1.5 eV,

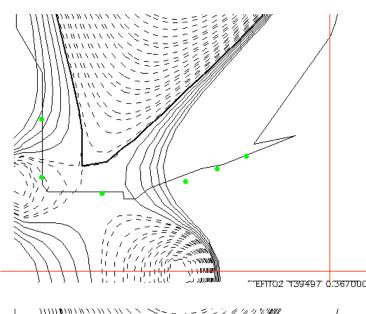
$$n_e \le 5 \times 10^{20} \text{ m}^{-3}$$

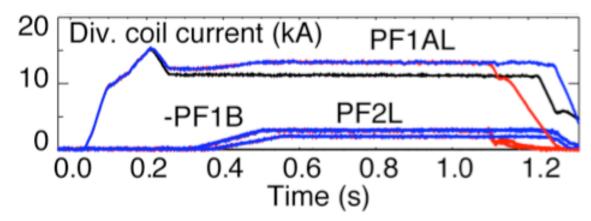
 Also suggests a reduction of carbon physical and chemical sputtering rates

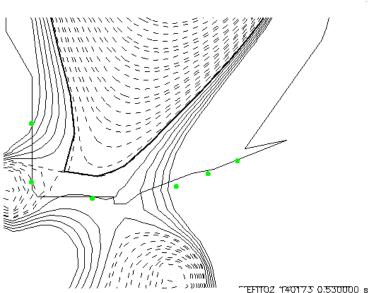




### Steady-state asymmetric snowflake-minus configuration has been obtained in FY2010 experiments in NSTX



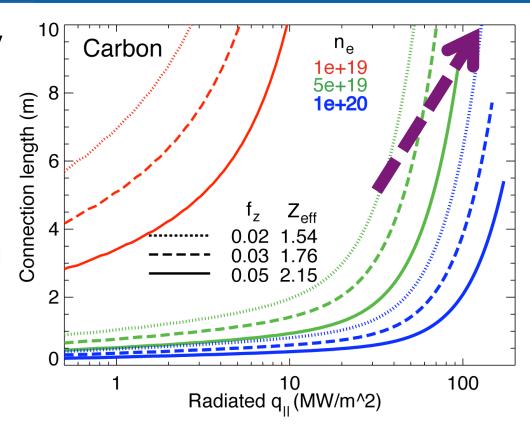




- Snowflake-minus with three coils (w/ reversed PF1B) transformed from a standard medium-δ LSN at ~ 500 ms
- Snowflake with three coils (w/ reversed PF1B) transformed from a standard high-δ LSN at ~ 500 ms

### 1D estimates indicate power and momentum losses are increased in snowflake divertor

- 1D divertor detachment model by Post
  - Electron conduction with noncoronal carbon radiation
  - Max  $q_{||}$  that can be radiated as function of connection length for range of  $f_z$  and  $n_e$
  - -> Greater fraction of  $q_{||}$  is radiated with increased  $L_x$
- Three-body electron-ion recombination rate depends on divertor ion residence time
  - Ion recombination time:  $\tau_{ion} \sim 1-10$  ms at  $T_e = 1.3 \text{ eV}$
  - Ion residence time:  $\tau_{ion} \le 3-6$  ms in standard divertor, x 2 in snowflake
  - -> Greater parallel momentum sink



$$q_{\parallel} = -\kappa_0 T_e^{5/2} \frac{\partial T_e}{\partial x}$$

$$\frac{\partial q_{\parallel}}{\partial x} = -n_e n_z L_Z(T_e)$$



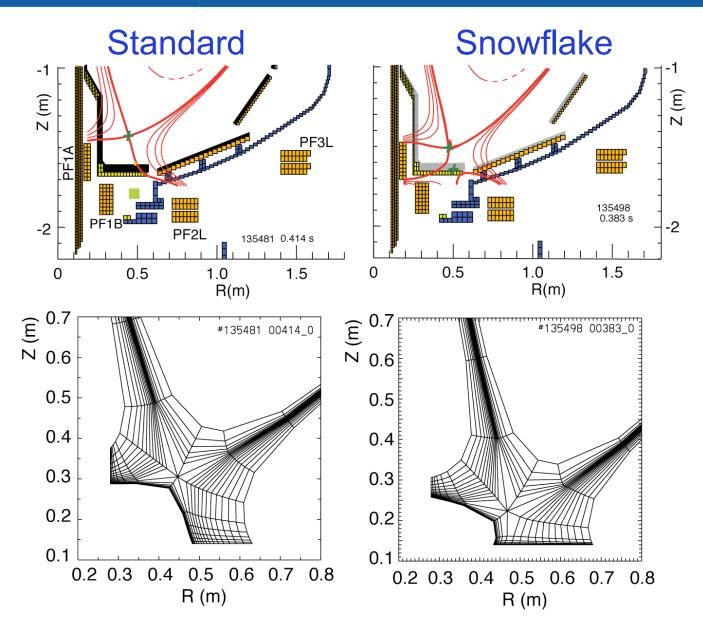
# 2D multi-fluid edge transport code UEDGE is used to study snowflake divertor properties

- Fluid (Braginskii) model for ions and electrons
- Fluid for neutrals
- Classical parallel transport, anomalous radial transport
- Core interface:

• 
$$T_e = 120 \text{ eV}$$

• 
$$n_e = 4.5 \times 10^{19}$$

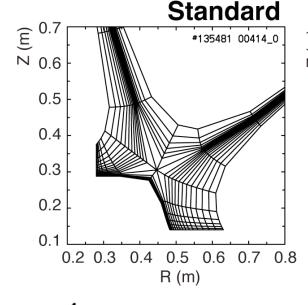
- $D = 0.25 \text{ m}^2/\text{s}$
- $\chi_{e,i} = 0.5 \text{ m}^2/\text{s}$
- $R_{recv} = 0.95$
- Carbon 3 %

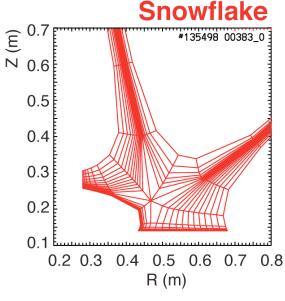


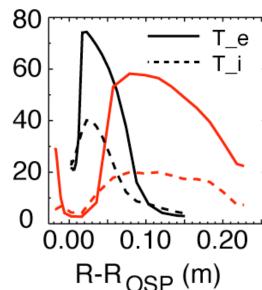


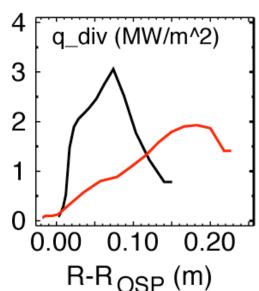
### 2D modeling shows a trend toward reduced temperature, heat and particle fluxes in the snowflake divertor

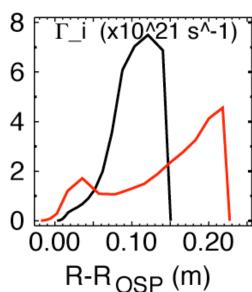
- 2D multi-fluid code UEDGE
  - Fluid (Braginskii) model for ions and electrons
  - Fluid for neutrals
  - Classical parallel transport, anomalous radial transport
    - $-D = 0.25 \text{ m}^2/\text{s}$
    - $-\chi_{e,i} = 0.5 \text{ m}^2/\text{s}$











Core interface:

•  $n_e = 4.5 \times 10^{19}$ 

 $R_{recv} = 0.95$ 

Carbon 3 %

